



POST-TENSIONING

DYWIDAG Multistrand PT System for Bonded Application with 3 to 55 strands ETA-13/0815





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European Technical Assessment

ETA-13/0815 of 29.01.2021

General part

Technical Assessment Body issuing the European Technical Assessment	Österreichisches Institut für Bautechnik (OIB) Austrian Institute of Construction Engineering
Trade name of the construction product	DYWIDAG Strand
Product family to which the construction product belongs	Bonded post-tensioning kits for prestressing of structures with 3 to 55 strands
Manufacturer	DYWIDAG-Systems International GmbH Neuhofweg 5 85716 Unterschleissheim Germany
Manufacturing plants	DYWIDAG-Systems International GmbH Max-Planck-Ring 1 40764 Langenfeld Germany
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This European Technical Assessment replaces	European Technical Assessment ETA-13/0815 of 25.06.2018.



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Remarks

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Specific parts

1 Technical description of the product

1.1 General

The European Technical Assessment¹ – ETA – applies to a kit, the bonded PT system

DYWIDAG Strand,

comprising the following components.

– Tendon

Bonded tendon with 3 to 55 tensile elements

- Tensile element

7-wire prestressing steel strand with nominal diameters and nominal tensile strengths as given in Table 1.

Nominal diameter		Designation according to prEN 10138-3 ²	Nominal tensile strength	
mm	inch		N/mm ²	
15.3	0.6	Y1770S7	1 770	
15.3	0.6	Y1860S7	1 860	
15.7	0.62	Y1770S7	1770	
15.7	0.62	Y1860S7	1 860	

Table 1Tensile elements

NOTE 1 N/mm² = 1 MPa

- Anchorage

Prestressing steel strand anchored by either 3-piece wedge or bond head.

Stressing (active) and fixed (passive) anchor with wedges, wedge plate, and multi-plane anchor body MA for tendons with 3 to 55 prestressing steel strands

ETA-13/0815 was firstly issued in 2013 as European technical approval with validity from 28.06.2013, converted 2018 to European Technical Assessment ETA-13/0815 of 25.06.2018 and amended 2021 to European Technical Assessment ETA-13/0815 of 29.01.2021.

Standards and other documents referred to in the European Technical Assessment are listed in Annex 30 and Annex 31.



Stressing (active) and fixed (passive) anchor with wedges and anchor plate SD for tendons with 3 to 9 prestressing steel strands

Fixed (passive) anchor with bond anchorage H for tendons with 3 to 22 prestressing steel strands

- Coupler

Prestressing steel strand anchored by 3-piece wedge.

Fixed coupler with wedges, coupler plate R, and multi-plane anchor body MA for tendons with 5 to 37 prestressing steel strands

Movable coupler with wedges and single strand couplers D for tendons with 3 to 37 prestressing steel strands

- Helix and additional reinforcement or only additional reinforcement without helix in the anchorage zone
- Ducts
- Permanent corrosion protection for tensile elements, anchors, and couplers

PT system

1.2 Designation and range of anchorages and couplers

1.2.1 Designation

Anchorages and couplers are designated by their function in the structure, the nominal diameter of the prestressing steel strands and the maximum number of the prestressing steel strands. The first number indicates the nominal diameter of the prestressing steel strand, "68" = 15.3 mm (0.6") or 15.7 mm (0.62"), followed by the maximum number of prestressing steel strands per unit "n", 68 n. The available anchorages and couplers are shown in Annex 1 and Annex 2, and are listed in Table 2.

Component		Number of strands ¹⁾						
Anchorage								
Wedge plate with anchor body MA			5		7		9	12 15 19 22 27 31 37 43 49 55
Anchor plate SD	3	4	5	6	7	8	9	
Bond anchorage H		4	5		7		9	12 15 19 22
Coupler								
Fixed coupler with coupler plate R and anchor body MA			5		7		9	12 15 19 22 27 31 37
Movable coupler D	3	4	5		7		9	12 15 19 22 27 31 37

Table 2	Anchorages and	Couplers
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⁰ One or more prestressing steel strands may be omitted to install tendons with numbers of prestressing steel strands between the numbers given.

"Multi-plane anchor body MA" and "anchor body MA" are synonyms.



1.2.2 Tendon range

The available tendon sizes are listed in Table 2. The characteristic values of maximum force of tendons are given in Annex 27.

Anchorage and coupler may be provided with less prestressing steel strands than the maximum number, resulting in a continuous tendon row. Thereby the prestressing steel strands are omitted as much as possible radial symmetrically. For all omitted prestressing steel strands, the respective bores in wedge plate or coupler plate do not need to be drilled. Alternatively, at wedge plate and coupler plate R a short length of prestressing steel strand with a wedge is pressed in. For coupler plate R the bores in the projecting collar may be equally redistributed. However, overall dimensions of wedge plate and coupler plate are unchanged in any case.

Moreover, each anchorage and coupler may be installed with virtually any meaningful number of prestressing steel strands smaller or equal to the complete number of prestressing steel strands for the respective size. However, the resulting prestressing force is exactly axial with regard to anchorage and coupler. This is obtained by an appropriate arrangement of the prestressing steel strands in wedge plate and coupler plate.

Anchorages and couplers with omitted strands are in any case installed with unchanged dimensions and unchanged reinforcement compared to anchorages and couplers with complete number of prestressing steel strands.

1.2.3 Anchorage

1.2.3.1 General

The stressing anchor arranges the prestressing steel strands for the stressing operation and subsequently anchors the stressed prestressing steel strands by means of wedges. Each prestressing steel strand is individually anchored within a conical bore of the wedge plate or anchor plate SD by means of a 3-piece wedge, see Annex 9. All prestressing steel strands of the bundle tendon are stressed at the same time.

At the fixed anchor, the prestressing steel strands are anchored by means of wedges in wedge plate or in anchor plate SD, or by bond and bond heads within bond anchorage H.

The same principles of anchorage apply from the smallest to the largest tendon.

1.2.3.2 Stressing and fixed anchor with wedge plate and anchor body MA

The stressing anchor comprises wedges, wedge plate, and multi-plane anchor body MA, see Annex 10 to Annex 13. The trumpet is arranged between anchor body MA and duct. Anchorage with anchor body MA can be installed without or with helix. The helix, if present, is centrically aligned to the anchor body MA and fastened in its position. If required, the free end of the helix is fastened to the additional reinforcement. The duct is inserted into the trumpet or screwed thereon. The wedge plate is slipped over the prestressing steel strands before stressing.

Anchorage with anchor body MA can be installed with a flat duct, see Annex 4.

The stressing anchor can also be used as a fixed anchor. In that case, access is given to the fixed anchor during stressing. If the fixed anchor is not accessible and embedded in concrete, the wedges are secured by a wedge keeper plate, see Annex 10.

1.2.3.3 Stressing and fixed anchor with anchor plate SD

The stressing anchor comprises wedges and anchor plate SD, see Annex 15 and Annex 16. The trumpet is fastened at the formwork, optionally with a connection tube. Duct and trumpet are joined by inserting the duct into the trumpet or the duct is screwed on the trumpet. The helix, if present, is centrically aligned to the trumpet and fastened in its position. If required, the free end of the helix is fastened to the additional reinforcement. The anchor plate SD is slipped over the strands before stressing.

Anchorage with anchor plate SD can be installed with a flat duct, see Annex 4.



The stressing anchor can also be used as a fixed anchor. In that case, access is given to the fixed anchor during stressing. If the fixed anchor is not accessible and embedded in concrete, the complete anchorage, comprising anchor plate SD, connection tube, trumpet, and helix is mounted at once and the wedges are secured in the anchor plate SD by means of a wedge keeper plate, see Annex 15.

1.2.3.4 Fixed anchor with bond anchorages H – HL and HR

At the fixed anchor with bond anchorage H, the prestressing steel strands are anchored by bond of the prestressing steel strands and in particular with bond heads to the structural concrete, see Annex 1, Annex 17, and Annex 18. Therefore, it can only be used as a fixed anchor, embedded in concrete. Beside bond heads, it comprises ring, helix, and spacers for creating the intended strand layout, see Annex 1 and Annex 17. The prestressing steel strands used in this anchorage are free of any surface treatment, i.e., free of temporary corrosion protection, neither applied at the manufacturing plant nor on site.

1.2.4 Coupler

1.2.4.1 General

In the coupler, the prestressing steel strands are anchored by means of wedges at both construction stages.

1.2.4.2 Fixed coupler with coupler plate R

The fixed coupler comprises wedges, coupler plate R and anchor body MA, see Annex 21 and Annex 22. The fixed coupler connects a 2nd tendon with an already stressed 1st tendon. The already stressed 1st tendon is anchored in the same way as a stressing anchor with wedge plate. In addition, the coupler plate R provides a projecting ring collar with conical bores and pre-installed wedges that are secured by press-on-segments and springs. The prestressing steel strands of the 2nd tendon are pushed into the bores from bottom side and anchored with pre-installed wedges.

A 100 mm long and at least 4 mm thick PE-HD insert is installed at the deviating point at the end of the trumpet if the coupler can be subjected to significant fatigue actions. The insert is not required for a plastic trumpet, where the duct is screwed on an external thread of the plastic trumpet.

1.2.4.3 Movable coupler D with single strand coupler

The movable coupler D comprises for each prestressing steel strand a single strand coupler. The single strand coupler is assembled of 2 wedges with 2 springs inside 2 barrel chucks, connected by the fitting bolt, see Annex 23. Movable couplers connect two tendons prior to stressing. The prestressing steel strands of both tendons are pushed into the single strand couplers and anchored with the pre-installed wedges. Springs between wedges and fitting bolt secure the wedge positions in the cones.

The group of single strand couplers are arranged staggered in up to 3 levels, see Annex 23 and Annex 24.

Prior to final assembly of the tube, and according to the stressing direction, the correct position of the coupler in the coupler tube is checked.

1.2.5 Centre and edge distances, concrete cover

All centre and edge distances have been determined with regard to requirements on load-bearing capacity, depending on the actual mean compressive strength of concrete at time of stressing, $f_{cm, 0}$. Distance of tendon anchorages conforms to the values specified in Annex 11, Annex 12, Annex 13, Annex 16, Annex 17, Annex 18, Annex 19, and Annex 20. However, these values for centre distance between anchorages may be reduced in one direction by 15 %, but not smaller than the outside diameter of the helix and the dimensions of anchor body MA or anchor plate SD



and placing of additional reinforcement is still possible. In case of a reduction of the distances in one direction, the centre and edge distances in the perpendicular direction are increased by the same percentage in order to keep an equal concrete area in the anchorage zone.

The concrete cover of tendons is neither smaller than 20 mm nor smaller than the concrete cover of reinforcement installed in the same cross section. Concrete cover at the anchorage is at least 20 mm on the grout cap. Standards and regulations on concrete cover in force at the place of use are observed.

1.2.6 Strength of concrete

Concrete according to EN 206 is used.

At the time of transmission of the prestressing force to the structural concrete, the actual mean cube compressive strength of concrete, $f_{cm, 0, cube}$, or the actual mean cylinder compressive strength of concrete, $f_{cm, 0, cyl}$, is at least as given in Annex 11, Annex 12, Annex 13, Annex 16, Annex 17, Annex 18, Annex 19, and Annex 20. The actual mean compressive strength, $f_{cm, 0, cube}$ or $f_{cm, 0, cyl}$, is verified by means of at least three specimens, cube of size 150 mm or cylinder with diameter of 150 mm and height of 300 mm, which are cured under the same conditions as the structure.

For partial prestressing with 30 % of the full prestressing force the actual mean compressive strength of concrete is at least $0.5 \cdot f_{cm, 0, cube}$ or $0.5 \cdot f_{cm, 0, cyl}$. Intermediate values may be interpolated linearly according to Eurocode 2.

1.2.7 Reinforcement in the anchorage zone

In any case, steel grades and dimensions of helix and additional reinforcement specified in Annex 11, Annex 12, Annex 13, Annex 16, Annex 17, Annex 18, Annex 19, Annex 20, and Annex 25 are conformed to.

The centric position of the helix, if present, is secured by welding the end ring onto the multiplane anchor body MA or onto the anchor plate SD or by means of holding devices that are braced against the tendon.

If required for a specific project design, the reinforcement given in Annex 11, Annex 12, Annex 13, Annex 16, Annex 17, Annex 18, Annex 19, and Annex 20 may be modified in accordance with the respective regulations in force at the place of use as well as with the relevant approval of the local authority and of the ETA holder to provide equivalent performance.

1.3 Designation and range of tendons

1.3.1 Designation

The tendon is designated by the nominal diameter of the prestressing steel strand and the number of prestressing steel strands with 68n. The first two digits indicate the nominal diameter of the prestressing steel strand "68" = 15.3 mm (0.6 ") or 15.7 mm (0.62 "), followed by two digits as the number "n" of prestressing steel strands, e.g. 6804.

1.3.2 Range of tendons

The PT system includes tendons, see Table 2, with 3 to 55 prestressing steel strands. Only 7wire prestressing steel strands with nominal diameters of 15.3 mm or 15.7 mm and tensile strengths of 1 770 N/mm² or 1 860 N/mm² are used. The dimensions and specifications of the prestressing steel strands are given in Table 1 and Annex 26.

Characteristic values of maximum force of the tendons are listed in Annex 27.

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1.3.3 Maximum stressing forces

Prestressing and overstressing forces are specified in the respective standards and regulations in force at the place of use. Annex 5 and Annex 6 list the maximum prestressing and overstressing forces of the tendons according to Eurocode 2. I.e., the maximum prestressing force applied to a tendon is not exceeding $P_{0, max} = 0.90 \cdot A_p \cdot f_{p0.1}$. Overstressing with up to $0.95 \cdot A_p \cdot f_{p0.1}$ is only permitted if the force in the prestressing jack can be measured to an accuracy of ± 5 % of the final value of the overstressing force.

Initial prestressing force, P_{m0} , immediately after stressing and anchoring does not exceed the forces as specified in Eurocode 2.

Where

A _p mm ²	Cross-sectional area of prestressing steel of tendon, i.e. $A_p = n \cdot S_0$
f _{p0.1} N/mm ²	Characteristic 0.1 % proof stress of prestressing steel, i.e. $F_{p0.1}$ = $f_{p0.1}\cdot S_0$
n	Number of prestressing steel strands, i.e. $n = 1$ to 55
S ₀ mm ²	Nominal cross-sectional area of one single prestressing steel strand, see Annex 26
F _{p0.1} kN	Characteristic value of 0.1 $\%$ proof force of one single prestressing steel strand, see Annex 26
P _{0, max} kN	Maximum prestressing force
P _{m0} kN	Initial prestressing force immediately after stressing and anchoring

1.4 Slip at anchorage and coupler

Slip at anchorage and coupler is taken into consideration in design and for determining tendon elongation. In Annex 14 slip and the required locking measure of wedges are specified.

1.5 Friction losses

The tendon layout should not feature abrupt changes of the tendon axis, since this may lead to significant additional friction losses. For calculation of losses of prestressing forces due to friction, Coulomb's friction law applies. Calculation of friction loss is by the equation

$$P_x = P_0 \cdot e^{-\mu \cdot (\alpha + k \cdot x)}$$

Where

Px	kN	Prestressing force at distance x from the stressing anchor along the tendon
P0	kN	Prestressing force at the distance $x = 0$ m
μ	rad ⁻¹	Friction coefficient, see Table 3
α	rad	Sum of angular deviations over a distance $\boldsymbol{x},$ irrespective of direction and sign
k	rad/m	Wobble coefficient, see Table 3
х	m	Distance along the tendon from the point where the prestressing force is equal to P_0

NOTE 1 rad = 1 m/m = 1



Table 3 Friction coefficient μ and wobble coefficient k

_		Circular	steel duct	Circular plastic duct		
		Duct I Duct II		Range	Recommended value	
μ	rad⁻1	0.20	0.19	0.10 to 0.14	0.14	
k	rad/m	0.005	0.005		0.005	
ĸ	°/m	(0.3) ¹⁾	(0.3) ¹⁾		(0.3) ¹⁾	

NOTE

¹⁾ For information only

For flat steel duct see Annex 4.

Information on friction losses in anchorages and couplers is included in Annex 3.

1.6 Support of ducts

Tendons are installed with high accuracy. This is achieved by installation of duct supports exactly levelled with regard to their designated position. The supports are secured in their position and the ducts fastened thereto. Distance between duct supports for tendons with steel strip sheaths does not exceed 1.80 m. In sections with maximum tendon curvature the distance between duct supports is reduced to 0.60 to 0.75 m.

If the prestressing steel strands are installed after concreting (duct II), special attention is applied that the duct will not displace. For that, the duct is additionally fastened between the supports e.g. to the reinforcement of the structure. If tendons are installed in several layers, only the lowest layer can be firmly connected with the duct support. All other tendon layers are placed and fastened on subsequently installed supports.

1.7 Radii of curvature

The minimum radii of curvature of tendons with steel strip sheaths as specified in Annex 7 and Annex 8 are observed. They correspond to

- A maximum prestressing force of the tendon of $P_{m0} = 0.85 \cdot F_{p0.1}$
- A nominal diameter of the prestressing steel strand of d = 15.7 mm
- Prestressing steel strand with a maximum nominal tensile strength of 1 860 N/mm²
- A maximum pressure under the prestressing steel strands of $p_{R, max}$ = 140 kN/m or 200 kN/m
- A minimum compressive strength of concrete of $f_{cm, 0, cube}$ = 25 N/mm²

In case of different tendon parameters or a different pressure under the prestressing steel strands, the calculation of the minimum radius of curvature can be carried out by the equation

$$R_{\min} = \frac{2 \cdot P_{m0} \cdot d}{d_i \cdot p_{R,\max}}$$

Where

R _{min} m	Minimum radius of curvature
P _{m0} kN	Prestressing force of the tendon
dmm	Nominal diameter of the prestressing steel strand
d _i mm	Inner duct diameter
p _{R. max} kN/m	Maximum pressure under the prestressing steel strands



The minimum radius of curvature should not be less than 2.0 m. For a reduction of the minimum radius of curvature, the effects of the radial deviation forces on the concrete and stresses resulting from the curvature in the prestressing steel require verification, or the stressing force is reduced accordingly. Standards and regulations on minimum radius of curvature or on the maximum pressure under the prestressing steel strands in force in the place of use are observed.

Components

1.8 Specification of prestressing steel strand

7-wire prestressing steel strand with plain surfaces of the individual wires, a nominal diameter of 15.3 or 15.7 mm and tensile strengths of 1770 N/mm² or 1860 N/mm² is used. Dimensions and specifications of the prestressing steel strand are according to prEN 10138-3 and are given in Clause 1.1, Table 1, and Annex 26.

In the course of preparing the European Technical Assessment, no characteristic has been assessed for the prestressing steel strand. In execution, a suitable prestressing steel strand that conforms to Annex 26 and is according to the standards and regulations in force at the place of use is taken.

1.9 Anchorage and coupler components

1.9.1 General

Specifications of anchorage and coupler components are given in the Annexes and the technical file³ of the European Technical Assessment. Therein the components' dimensions, materials, material identification data with tolerances and the materials used in corrosion protection are specified.

For prestressing steel strands with nominal tensile strength of 1 860 N/mm² as well as 1 770 N/mm² the same anchorages and couplers are used.

1.9.2 Wedge plate and anchor plate SD

Both, wedge plate and anchor plate SD are made of steel with a pattern of regular arranged bores for anchoring the prestressing steel strands, see Annex 9, Annex 11, Annex 12, Annex 13, Annex 16, and Annex 22. The bores are cylindrical with conical ends at one side for bearing the wedges and are identical for stressing and fixed anchors. All bores are countersunk and deburred. See Annex 9 for details on the conical bores.

The wedge plate is supported by anchor body MA for load transfer to the structural concrete. Anchor plate SD serves for both in one piece, anchoring the prestressing steel strands and load transfer to the structural concrete by one load transfer plane.

For installation the bores and cones are clean and free of damage or rust and are provided with corrosion protection oil.

1.9.3 Coupler plate R

The coupler plate R for fixed couplers, see Annex 22, is made of steel with two patterns of regular arranged bores for anchoring the prestressing steel strands. In the inner part of the coupler plates, the pattern is identical with the pattern of the wedge plate, providing cylindrical bores with conical ends at one side for bearing the wedges of the 1st construction stage. On the outer ring collar of the coupler plate, the pattern of bores are concentric rings, providing cylindrical bores with conical ends at one side for bearing the wedges of the 2nd construction stage. All bores are countersunk and deburred. See Annex 9 for details on the conical bores.

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³ The technical file of the European Technical Assessment is deposited at Österreichisches Institut für Bautechnik.



At the 2nd construction stage, the wedges are pre-installed in the conical bores and secured with springs. A grouting box with vent is attached to coupler plate R to facilitate grouting.

For installation the bores and cones are clean and free of damage or rust and are provided with corrosion protection oil.

1.9.4 Multi-plane anchor body MA

Multi-plane anchor body MA, see Annex 11, Annex 12, and Annex 13 is made of cast iron and used together with wedge plate as stressing or fixed anchor and with coupler plates R as fixed coupler.

Anchor body MA is of circular shape and provides several load transfer planes for load transfer to concrete. A centric circular hole allows for passing through the tendon.

1.9.5 Single strand coupler

The single strand coupler, see Annex 23, is made of steel and employed for movable coupler D. Single strand coupler comprises 2 barrel chucks with conical bore and inner thread, 2 wedges, and 2 springs. The barrel chucks are connected by screwing a fitting bolt in steel in the inner threads of both barrel chucks.

For installation, the prestressing steel strands of both tendons are pushed into the single strand coupler with pre-assembled wedges, locked with springs. Cones are clean and free of damage or rust and provided with corrosion protection oil.

1.9.6 Bond head

The bulb shaped bond head at the end of the prestressing steel strand, see Annex 17, for bond anchorage H is made by means of a special jack.

1.9.7 Ring

Steel ring is used for bond anchorage H, see Annex 17, Annex 19, and Annex 20.

1.9.8 Wedges

Only 3-piece wedges according to Annex 9 are used. The wedges feature different lengths for the respective nominal diameters of the prestressing steel strand, see Annex 9.

1.9.9 Wedge keeper plate

Wedge keeper plate is used for fixed anchor that is not accessible, either with wedge plate, see Annex 10, or with anchor plate SD, see Annex 15.

1.10 Helix and additional reinforcement

Steel grades and dimensions of helix and additional reinforcement conform to the specifications given in the Annexes and the technical file of the European Technical Assessment. Helix for anchorage with anchor bodies MA can be made of plain round steel wire or ribbed reinforcing steel. Helix for bond anchorage H is made of ribbed reinforcing steel. Generally, both ends of each helix are welded to closed rings. Welding of one end, the inner end, may be omitted. Details on welding of helix are given in Annex 11, Annex 12, and Annex 16.

1.11 Duct

Usually, a corrugated duct made of steel strips is used. As a general rule, ducts with a smaller inner diameter, duct I, are used for pre-fabricated tendons. Longer tendons are transported to the job site in coils or oblong loops. The minimum transport bending diameter D for tendons up to 6812 is 1.50 m and for larger tendons up to 6827 is 1.80 m.

For on-site fabrication of tendons, the prestressing steel strands are inserted into the ducts either before or after placing the concrete. In general, ducts with a larger inner diameter, duct II, are used



for that purpose. Either one or several prestressing steel strands are consecutively pushed or pulled into the respective duct or the entire tendon all at once.

In general, the ducts have circular cross section – so called "round" duct. Optionally, for tendons 6803 to 6805, ducts with oval cross sections – so called "flat" duct – are available. The ends of the ducts are connected with couplers. For length compensation, a short duct piece may be installed between duct and trumpet of an anchorage as a telescopic duct.

The circular duct conforms to EN 523. For the flat duct EN 523 applies analogously.

Alternatively, corrugated plastic ducts may be installed, if permitted at the place of use.

1.12 Permanent corrosion protection

In the course of preparing the European Technical Assessment no characteristic has been assessed for components and materials of the corrosion protection system. In execution, all components and materials are selected according to the standards and regulations in force at the place of use.

Corrosion protection of tendon, anchorage, and coupler is provided by grout according to EN 447, special grout according to EAD 160027-00-0301, or ready-mixed grout with an adequate composition according to standards and regulations in force at the place of use.

1.13 Welding

Welding is only permitted for the following components.

- Welding the helix end turn to a closed ring.
- Welding the helix end ring to the anchor body MA or to the anchor plate SD or its connection tube to secure the centric position of the helix.

During welding it is ensured that there is no contact to duct and to prestressing steel strand.

After assembly of the tendons, no welding operations are carried out anymore. Welding operations close to tendons require precautionary measures to avoid damage.

1.14 Material specifications of the components

Material specifications of the components are given in Annex 25.

2 Specification of the intended use in accordance with the applicable European Assessment Document (hereinafter EAD)

2.1 Intended use

The PT system DYWIDAG Strand is intended to be used for the prestressing of structures. The specific intended use is

- Internal bonded tendon for concrete and composite structures

2.2 Assumptions

2.2.1 General

Concerning product packaging, transport, storage, maintenance, replacement, and repair it is the responsibility of the manufacturer to undertake the appropriate measures and to advise his clients on transport, storage, maintenance, replacement, and repair of the product as he considers necessary.



2.2.2 Packaging, transport and storage

Tendons and anchorages may be assembled on site or at the factory, i.e. pre-assembled tendons.

The tendons are packed, stored, and transported in transport racks, pallets, and bobbins such that they do not fall short of the following curvature diameters D.

For tendons up to $6812\ldots D \geq 1.50~m$

For larger tendons up to $6827 \dots D \ge 1.80 \text{ m}$

Advice on packaging, transport, and storage includes.

- Temporary protection of prestressing steels and components in order to prevent corrosion during transportation from the production site to the job site
- Transportation, storage, and handling of prestressing steel and other components in a manner as to avoid damage by mechanical or chemical impact
- Protection of tensile elements and other components from moisture
- Keeping tensile elements away from zones where welding operations are performed

2.2.3 Design

2.2.3.1 General

Advice on design includes the following items.

Design of the structure permits correct installation, stressing, and grouting of tendon and design and reinforcement of the anchorage zone permits correct placing and compacting of concrete.

Tendons arranged one on top of each other are separated by an appropriate thick concrete layer, as in case of tendon curvatures there is a risk of inner ducts being crushed as a result of deviation forces from the prestressed outer tendons.

Verification of transfer of prestressing forces to the structural concrete is not required, if centre and edge distances of the tendons, strength of concrete, as well as grade and dimensions of helix and additional reinforcement, see Clause 1.2.5, Clause 1.2.6, Clause 1.2.7, Annex 11, Annex 12, Annex 13, Annex 16, Annex 17, Annex 18, Annex 19, and Annex 20, are conformed to. The forces outside the area of helix and additional reinforcement are verified and, if necessary, covered by appropriate, in general transverse reinforcement. The reinforcement of the structure is not employed as additional reinforcement. Reinforcement exceeding the required reinforcement of the structure may be used as additional reinforcement if appropriate placing is possible.

If required for a specific project design, the reinforcement given in Annex 11, Annex 12, Annex 13, Annex 16, Annex 17, Annex 18, Annex 19, and Annex 20 may be modified in accordance with the respective regulations in force at the place of use as well as with the relevant approval of the local authority and of the ETA holder to provide equivalent performance.

The anchor recess is designed as to ensure a concrete cover of at least 20 mm at the grout caps in the final state.

The initial prestressing force applied to the stressing anchor will decrease especially as a result of slip, see Clause 1.4 and Annex 14, of friction along the tendon, see Clause 1.5, and of the elastic shortening of the structure, and in the course of time because of relaxation of the prestressing steel, and creep and shrinkage of concrete. The stressing instructions prepared by the ETA holder should be consulted.



2.2.3.2 Bond anchorage

For calculation of elongations the free length of the tendon includes 50 % of the distance between ring and bond head. Full tendon force is applied after the ring only. Between ring and bond head the decrease of the tendon force can be assumed to be linear and zero at the beginning of the bond head.

2.2.3.3 Increased losses of prestressing forces at fixed coupler

For verification of the limitation of crack widths and for verification of the stress range increased losses of prestressing forces at fixed couplers due to creep and shrinkage of the concrete are taken into consideration. The determined losses of prestressing forces of tendons without the influence of couplers are multiplied by the factor 1.5 in the areas of fixed couplers.

For movable couplers, increased losses of prestressing forces do not need to be taken into consideration.

2.2.3.4 Fixed coupler

Under all possible load combinations, the prestressing force at the 2nd construction stage of the fixed coupler is at no time higher than at the 1st construction stage, neither during construction nor in the final state.

2.2.3.5 Movable coupler

The length of the coupler tube and its position relative to the coupler ensures unimpeded movement of the coupler in the coupler tube along a length of $\geq \max \begin{cases} 1.20 \cdot \Delta I \\ 120 \text{ mm} \end{cases}$, with ΔI in mm as the expected displacement of the coupler during stressing.

2.2.3.6 Tendons in masonry structures

Post-tensioning kits are primarily used in structures made of concrete. They can, however, be used with other structural materials, e.g. in masonry structures. However, there is no particular assessment in EAD 160004-00-0301 for these applications. Hence, load transfer of stressing force from the anchorage to the masonry structure is via concrete or steel member, designed according to the European Technical Assessment, especially according to the Clauses 1.2.5, 1.2.6, 1.2.7, or Eurocode 3 respectively.

The concrete or steel members have such dimensions as to permit a force of $1.1 \cdot F_{pk}$ being transferred into the masonry. The verification is performed according to Eurocode 6 as well as to the respective standards and regulations in force at the place of use.

2.2.4 Installation

2.2.4.1 General

It is assumed that the product will be installed according to the manufacturer's instructions or – in absence of such instructions – according to the usual practice of the building professionals.

Assembly and installation of tendons are only carried out by qualified PT specialist companies with the required resources and experience in the use of bonded multi-strand post-tensioning systems, see CWA 14646. The company's PT site manager has a certificate, stating that she or he has been trained by the ETA holder and that she or he possesses the necessary qualification and experience with the PT system DYWIDAG Strand.

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2.2.4.2 Anchorages

2.2.4.2.1 General

Stressing and fixed anchor with anchor body MA and wedge plate, fixed coupler with anchor body MA and coupler plate R, and stressing and fixed anchor with anchor plate SD are installed perpendicular to the tendon's axis. Adjacent to the trumpet, the tendon continues with a straight section over a length of at least 250 mm.

The centric position of the helix is secured by welding the end ring to anchor body MA or to the anchor plate SD or its connection tube or by means of spacers braced against the tendon. The additional reinforcement is fastened centrically to the trumpet by tying or by means of spacers.

2.2.4.2.2 Stressing anchor

Site assembly comprises the following working steps, see Annex 10 and Annex 15.

- Fastening the anchor body MA or trumpet or connection tube for anchor plate SD to the formwork.
- Installation of the trumpet between anchor body MA and duct or between connection tube for anchor plate SD and duct.
- If the helix is not already welded onto the anchor body MA or the connection tube for anchor plate SD in the manufacturing plant, the helix is placed, centred relative to the tendon axis and fastened to the reinforcement.
- Pushing the duct into the trumpet to approximately a length of d, with d as the duct diameter, or aligning trumpet and duct and connecting them by means of a duct coupler with a minimum length of 2 · d, or, in the case of appropriately shaped plastic trumpets, screwing the duct onto the trumpet.
- Sealing the joint trumpet to duct.
- Pushing the wedge plate or the anchor plate SD over the strands shortly before stressing.
- Tightening the prestressing steel strands with 3-piece wedges.

2.2.4.2.3 Fixed anchor

The anchorage with anchor body MA and wedge plate or with anchor plate SD is also used as fixed anchor. If the fixed anchor is accessible during stressing, the installation is the same as for the stressing anchor according to Clause 2.2.4.2.2 with an anchor body MA with wedge plate or an anchor plate SD.

If the fixed anchor is not accessible during stressing, site assembly comprises the following working steps, see Annex 10 and Annex 15.

- Assembly and placing of multi-plane anchor body MA, helix, trumpet, and duct or of connection tube, trumpet, and duct at the formwork. Subsequently fastening of respective components to reinforcement and sealing of joints.
- Pushing or pulling of strands.
- Pushing the wedge plate or the anchor plate SD over the strands.
- Installation of wedges and pre-wedging with P_{0, max} according to Annex 5 and Annex 6 and subsequently securing the wedges with a wedge keeper plate.
- Mounting of grout cap together with respective sealing and vent pipes.

2.2.4.2.4 Bond anchorage H – HL or HR

Before shaping the bond heads, ring, helix, and spacers are placed on the tendon. The bond heads are shaped in the manufacturing plant or on site by cold forming and all bond heads are arranged by means of spacers according to their designated position.



2.2.4.3 Couplers

2.2.4.3.1 Fixed coupler with coupler plate R

The fixed coupler R joints a 2nd tendon with an already stressed 1st tendon. The anchorage of the prestressing steel strands in the already stressed 1st tendon in coupler plate R is equivalent to the stressing anchor with wedge plate and anchor body MA. The coupler with coupler plate R and anchor body MA are installed perpendicular to the tendon's axis with the same procedure as the stressing anchor. Adjacent to the trumpet, the tendon continues with a straight section over a length of at least 250 mm.

Site assembly of the 2nd tendon comprises the following working steps, see Annex 21 and Annex 22.

- Assembly and positioning of end trumpet, duct sleeve, and duct in the formwork, subsequently fastening of respective components to reinforcement and sealing of the joints. End trumpet and duct sleeve are mounted with distance L_t from coupler plate R, where L_t as the total length of the end trumpet.
- Pushing or pulling of strands.
- Jointing the 2nd tendon with the 1st tendon by inserting the strands into the cylindrical bores of the outer ring collar of coupler plate R. The strands are locked by the pre-installed wedges, springs and press-on-segments at the rear conical ends of the cylindrical bores. Proper seating of the strand ends with regard to sufficient insertion length is checked with colour markings. The section behind the conical ends of the outer ring collar is covered with an also pre-installed protection cap.
- Installing end trumpet and duct sleeve in final position.
- Arranging grout or vent pipes on end trumpet and on protection cap for grouting.
- 2.2.4.3.2 Movable coupler with single strand couplers D

The movable coupler joints two tendons prior to stressing by single strand couplers. The strands of both tendons are anchored by means of wedges. The single strand couplers consist of 2 coupler barrel chucks each with cone and thread, which are connected by a steel fitting bolt. Springs between wedges and fitting bolt secure the wedge positions in the cones.

Site assembly of the coupler D comprises the following working steps, see Annex 23 and Annex 24.

- Assembly and positioning of duct, sleeve tubes, trumpets, and coupler tube at the formwork. Subsequently, fastening of duct to reinforcement and sealing of the joints. Coupler tube, trumpets and sleeve tubes remain pushed back on duct, to provide space for installation of strand couplers.
- Pushing or pulling of strands.
- Cutting to length of strand with regard to staggered position of single strand couplers.
- Connecting the strands with strand couplers D by inserting the strand into the bores of the single strand couplers. The proper seating of the two strand ends with regard to sufficient insertion length is checked with colour markings.
- Before final assembly of coupler tube, trumpets, and sleeve tubes, checking the correct position of single strand couplers in the coupler tube with regard to the direction of stressing.
- Installing of coupler tube, trumpets and sleeve tube and sealing the joints.
- Arranging a vent pipe at both ends of the coupler tube.



2.2.4.4 Ducts and tendon placement

Tendons are installed with high accuracy on supports, see Clause 1.6. During installation careful handling of tendons is ensured.

Prior to concreting, the PT site manager carries out a final examination of the installed tendons. Damages to duct or tendons are either repaired immediately or reported to the responsible person.

2.2.4.5 Stressing and stressing records

2.2.4.5.1 Stressing

With a mean compressive strength of concrete in the anchorage zone according to Annex 11, Annex 12, Annex 13, Annex 16, Annex 19, and Annex 20 full prestressing may be performed.

The prestressing forces are applied in accordance with a prescribed stressing schedule. Said schedule includes

- Mean cube or cylinder compressive strength of the concrete at time of stressing
- Time and sequence of the various prestressing levels
- Prestressing forces and elongations calculated for the tendons
- Time and kind of shuttering lowering and removal
- Any possible spring back forces of the falsework are taken into account.

2.2.4.5.2 Restressing

Restressing of tendons in combination with release and reuse of wedges is permitted. After restressing the wedges bite into a least 15 mm of virgin strand surface and no wedge marks remain on the tendon between the anchorages.

Stressing records

For each tendon any important observation made during the stressing operation, in particular prestressing forces applied, and elongation measured, are recorded in stressing records.

2.2.4.5.3 Stressing equipment, clearance requirements, and safety-at-work

For stressing, hydraulic jacks are used. Information about the stressing equipment has been submitted to Österreichisches Institut für Bautechnik.

To stress the tendons, clearance of approximately 1 m directly behind the anchorages is ensured. The ETA holder keeps available more detailed information on prestressing jacks used and the required space for handling and stressing.

The safety-at-work and health protection regulations shall be complied with.

2.2.4.6 Grouting of tendons

2.2.4.6.1 Grout

Grout according to EN 447, special grout according to EAD 160027-00-0301, or ready-mixed grout with an adequate composition according to standards and regulations in force at the place of use is used.

2.2.4.6.2 Grouting procedure

All anchorages have inlets and vents for grouting or ventilation. The ducts have vent pipes at their top points and at additional points, if required.

After completion of the prestressing operation and acceptance of the stressing records, the tendons are grouted as soon as possible. For the grouting procedure, EN 446 applies. Standards and regulations in force at the place of use are observed. If tendons remain



ungrouted for a longer time, appropriate corrosion protection measures are implemented after acceptance of the ETA holder.

The anchor recesses are concreted once stressing and grouting are completed, to establish a complete corrosion protection of the tendon.

2.3 Assumed working life

The European Technical Assessment is based on an assumed working life of DYWIDAG Strand of 100 years, provided that DYWIDAG Strand is subject to appropriate installation, use, and maintenance, see Clause 2.2. These provisions are based upon the current state of the art and the available knowledge and experience.

In normal use conditions, the real working life may be considerably longer without major degradation affecting the basic requirements for construction works⁴.

The indications given as to the working life of the construction product cannot be interpreted as a guarantee, neither given by the product manufacturer or his representative nor by EOTA nor by the Technical Assessment Body but are regarded only as a means for expressing the expected economically reasonable working life of the product.

3 Performance of the product and references to the methods used for its assessment

3.1 Essential characteristics

The performances of DYWIDAG Strand for the essential characteristics are given in Table 4.

Nº	Essential characteristic	Product performance			
	Basic requirement for construction work	s 1: Mechanical resistance and stability			
1	Resistance to static load	See Clause 3.2.1.1.			
2	Resistance to fatigue	See Clause 3.2.1.2.			
3	Load transfer to the structure	See Clause 3.2.1.3.			
4	Friction coefficient	See Clause 3.2.1.4.			
5	Deviation, deflection (limits) for internal bonded and internal unbonded tendon	See Clause 3.2.1.5.			
6	Assessment of assembly	See Clause 3.2.1.6.			
7	Corrosion protection	See Clause 3.2.1.7.			
	Basic requirement for construction	on works 2: Safety in case of fire			
8	Reaction to fire	See Clause 3.2.2.1.			

 Table 4
 Essential characteristics and performances of the product

The real working life of a product incorporated in a specific works depends on the environmental conditions to which that works are subject, as well as on the particular conditions of design, execution, use, and maintenance of that works. Therefore, it cannot be excluded that in certain cases the real working life of the product may also be shorter than the assumed working life.



N⁰	Essential characteristic	Product performance								
	Basic requirement for construction works	3: Hygiene, health, and the environment								
9	Content, emission, and/or release of dangerous substances	See Clause 3.2.3.1.								
	Basic requirement for construction works 4: Safety and accessibility in use									
	 Not relevant. No characteristic assessed. 									
	Basic requirement for construction	works 5: Protection against noise								
	Not relevant. No characteristic assessed.									
	Basic requirement for construction work	s 6: Energy economy and heat retention								
	Not relevant. No characteristic assessed.									
	Basic requirement for construction works	s 7: Sustainable use of natural resources								
	No characteristic assessed.									

3.2 Product performance

- 3.2.1 Mechanical resistance and stability
- 3.2.1.1 Resistance to static load

The PT system as described in the ETA meets the acceptance criteria of EAD 160004-00-0301, Clause 2.2.1. The characteristic values of maximum force, F_{pk} , of the tendon with prestressing steel strands according to Annex 26 are listed in Annex 27.

3.2.1.2 Resistance to fatigue

The PT system as described in the ETA meets the acceptance criteria of EAD 160004-00-0301, Clause 2.2.2. The characteristic values of maximum force, F_{pk} , of the tendon with prestressing steel strands according to Annex 26 are listed in Annex 27.

Fatigue resistance of anchorages and couplers was tested and verified with an upper force of $0.65 \cdot F_{pk}$, a fatigue stress range of 80 N/mm², and $2 \cdot 10^6$ load cycles.

3.2.1.3 Load transfer to the structure

The PT system as described in the ETA meets the acceptance criteria of EAD 160004-00-0301, Clause 2.2.3. The characteristic values of maximum force, F_{pk} , of the tendon with prestressing steel strands according to Annex 26 are listed in Annex 27.

Conformity with the stabilisation and crack width criteria specified for the load transfer test was verified to a force level of $0.80 \cdot F_{pk}$.

3.2.1.4 Friction coefficient

For friction losses including friction coefficient see Clause 1.5.

3.2.1.5 Deviation, deflection (limits) for internal bonded and internal unbonded tendon For minimum radii of curvature see Clause 1.7.



3.2.1.6 Assessment of assembly

The PT system as described in the ETA meets the acceptance criteria of EAD 160004-00-0301, Clause 2.2.7.

3.2.1.7 Corrosion protection

The PT system as described in the ETA meets the acceptance criteria of EAD 160004-00-0301, Clause 2.2.13.

3.2.2 Safety in case of fire

3.2.2.1 Reaction to fire

The performance of components made of steel or cast iron is Class A1 without testing.

The performance of components of other materials has not been assessed.

3.2.3 Hygiene, health, and the environment

3.2.3.1 Content, emission and/or release of dangerous substances

According to the manufacturer's declaration, the PT system does not contain dangerous substances.

SVOC and VOC

The performance of components made of steel or cast iron that are free of coating with organic material is no emission of SVOC and VOC.

The performance of components of other materials has not been assessed.

- Leachable substances

The product is not intended to be in direct contact to soil, ground water, and surface water.

3.3 Assessment methods

The assessment of the essential characteristics in Clause 3.1 of DYWIDAG Strand, for the intended use, and in relation to the requirements for mechanical resistance and stability, safety in case of fire, and for hygiene, health and the environment, in the sense of the basic requirements for construction works Nº 1, 2, and 3 of Regulation (EU) Nº 305/2011, has been made in accordance with Annex A of EAD 160004-00-0301, Post-tensioning kits for prestressing of structures, for Item 1, Internal bonded tendon.

3.4 Identification

The European Technical Assessment for DYWIDAG Strand is issued on the basis of agreed data that identify the assessed product⁵. Changes to materials, to composition, or to characteristics of the product, or to the production process could result in these deposited data being incorrect. Österreichisches Institut für Bautechnik should be notified before the changes are introduced, as an amendment of the European Technical Assessment is possibly necessary.



4 Assessment and verification of constancy of performance (hereinafter AVCP) system applied, with reference to its legal base

4.1 System of assessment and verification of constancy of performance

According to Commission Decision 98/456/EC, the system of assessment and verification of constancy of performance to be applied to DYWIDAG Strand is System 1+. System 1+ is detailed in Commission Delegated Regulation (EU) № 568/2014 of 18 February 2014, Annex, point 1.1., and provides for the following items.

- (a) The manufacturer shall carry out
 - (i) factory production control;
 - (ii) further testing of samples taken at the manufacturing plant by the manufacturer in accordance with the prescribed test plan⁶.
- (b) The notified product certification body shall decide on the issuing, restriction, suspension, or withdrawal of the certificate of constancy of performance of the construction product on the basis of the outcome of the following assessments and verifications carried out by that body
 - an assessment of the performance of the construction product carried out on the basis of testing (including sampling), calculation, tabulated values, or descriptive documentation of the product;
 - (ii) initial inspection of the manufacturing plant and of factory production control;
 - (iii) continuing surveillance, assessment, and evaluation of factory production control;
 - (iv) audit-testing of samples taken by the notified product certification body at the manufacturing plant or at the manufacturer's storage facilities.

4.2 AVCP for construction products for which a European Technical Assessment has been issued

Notified bodies undertaking tasks under System 1+ shall consider the European Technical Assessment issued for the construction product in question as the assessment of the performance of that product. Notified bodies shall therefore not undertake the tasks referred to in Clause 4.1, point (b) (i).

5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable EAD

5.1 Tasks for the manufacturer

5.1.1 Factory production control

The kit manufacturer exercises permanent internal control of the production. All the elements, procedures, and specifications adopted by the kit manufacturer are documented in a systematic manner in the form of written policies and procedures.

- Control of the incoming materials

The manufacturer checks the incoming materials to establish conformity with their specifications.

The prescribed test plan has been deposited with Österreichisches Institut für Bautechnik and is handed over only to the notified product certification body involved in the procedure for the assessment and verification of constancy of performance. The prescribed test plan is also referred to as control plan.



Inspection and testing

Kind and frequency of inspections, tests, and checks conducted during production and on the final product normally include.

- Definition of the number of samples taken by the kit manufacturer
- Material properties e.g. tensile strength, hardness, surface finish, chemical composition, etc.
- Determination of the dimensions of components
- Check correct assembly
- Documentation of tests and test results

All tests are performed according to written procedures with suitable calibrated measuring devices. All results of inspections, tests, and checks are recorded in a consistent and systematic way. The basic elements of the prescribed test plan are given in Annex 28, conform to EAD 160004-00-0301, Table 3, and are specified in the quality management plan of the DYWIDAG Strand.

The results of inspections, tests, and checks are evaluated for conformity. Shortcomings request the manufacturer to immediately implement measures to eliminate the defects.

- Control of non-conforming products

Products, which are considered as not conforming to the prescribed test plan, are immediately marked and separated from such products that do conform. Factory production control addresses control of non-conforming products.

- Complaints

Factory production control includes procedures to keep records of all complaints about the PT system.

The records are presented to the notified product certification body involved in continuous surveillance and are kept at least for ten years after the product has been placed on the market. On request, the records are presented to Österreichisches Institut für Bautechnik.

At least once a year the manufacturer audits the manufacturers of the components given in Annex 29.

5.1.2 Declaration of performance

The manufacturer is responsible for preparing the declaration of performance. When all the criteria of the assessment and verification of constancy of performance are met, including the certificate of constancy of performance issued by the notified product certification body, the manufacturer draws up the declaration of performance. Essential characteristics to be included in the declaration of performance for the corresponding intended use are given in Table 4.

5.2 Tasks for the notified product certification body

5.2.1 Initial inspection of the manufacturing plant and of factory production control

The notified product certification body establishes that, in accordance with the prescribed test plan, the manufacturing plant, in particular personnel and equipment, and the factory production control are suitable to ensure a continuous manufacturing of the PT system according to the given technical specifications. For the most important activities, EAD 160004-00-0301, Table 4 summarises the minimum procedure.



5.2.2 Continuing surveillance, assessment, and evaluation of factory production control

The activities are conducted by the notified product certification body and include surveillance inspections. The kit manufacturer is inspected at least once a year. Factory production control is inspected, and samples are taken for independent single tensile element tests.

For the most important activities, the control plan according to EAD 160004-00-0301, Table 4 summarises the minimum procedure. It is verified that the system of factory production control and the specified manufacturing process are maintained, taking account of the control plan.

Each manufacturer of the components given in Annex 29 is audited at least once in five years. It is verified that the system of factory production control and the specified manufacturing process are maintained, taking account of the prescribed test plan.

The results of continuous surveillance are made available on demand by the notified product certification body to Österreichisches Institut für Bautechnik. When the provisions of the European Technical Assessment and the prescribed test plan are no longer fulfilled, the certificate of constancy of performance is withdrawn by the notified product certification body.

5.2.3 Audit-testing of samples taken by the notified product certification body at the manufacturing plant or at the manufacturer's storage facilities

During surveillance inspection, the notified product certification body takes samples of components of the PT system for independent testing. Audit-testing is conducted at least once a year by the notified product certification body. For the most important components, Annex 29 summarises the minimum procedures. Annex 29 conforms to EAD 160004-00-0301, Table 4. In particular, at least once a year, the notified product certification body also carries out one single tensile element test series according to EAD 160004-00-0301, Annex C.7 and Clause 3.3.4 on specimens taken from the manufacturing plant or at the manufacturer's storage facility.

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The original document is signed by

Rainer Mikulits Managing Director Page 28 of European Technical Assessment ETA-13/0815 of 29.01.2021, replaces European Technical Assessment ETA-13/0815 of 25.06.2018





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Tendon 6803 6804 6805 6807 6808 6809 6812 6815 Number of strands 3 4 5 6 7 8 9 12 15 Cross-sectional area ⊘ 15.7 mm mm² 420 560 700 840 980 1120 1280 1800 2250 Nominal mass of prestressing steel ⊘ 15.7 mm kg/m 3.28 4.37 5.47 6.56 7.03 8.20 9.37 10.55 14.06 17.58 Modulus of elasticity N/mm²	Те	chnical data	a for te		0000	10 000	5 WIUI	Tourio	1 3100	adot					
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Tendon			6803	6804	6805	6806	6807	680	8 6809	6812	6815			
$\begin{array}{c} \mbox{Cross-sectional area}{$>$ 15.3 mm mm^2$ 420 560 700 840 980 1120 1260 1680 2100 of prestressing steel $$>$ 15.7 mm mm^2$ 450 600 750 900 1050 1200 1350 1800 2250 $$$ Nominal mass of $$>$ 15.3 mm kg/m$ 3.28 4.37 5.47 6.56 7.03 8.20 9.37 10.55 14.06 17.58 $$$ Modulus of elasticity $$$ N/mm^2$ 195 000 (standard value)$$$$ Modulus of elasticity $$$ N/mm^2$ 195 000 (standard value)$$$$$ Modulus of elasticity $$$$ N/mm^2$ 195 000 (standard value)$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$	Number of strands			3	4	5	6	7	8	9	12	15			
of prestressing steel ⊘ 15.7 mm mm² 450 600 750 900 1050 1200 1350 1800 2250 Nominal mass of ⊘ 15.7 mm kg/m 3.28 4.37 5.47 6.56 7.65 8.74 9.84 13.12 16.40 prestressing steel ⊘ 15.7 mm kg/m 3.52 4.69 5.86 7.03 8.20 9.37 10.55 14.06 17.58 Modulus of elasticity N/mm² 195000 (standard value) 76 10 9 10 10 Duct I Ø d/da mm 45/52 50/57 55/62 60/67 60/67 70/77 70/77 80/87 85/92 Eccentricity mm 5 9 10 11 9 14 12 14 13 Distance of tendon support m 5 9 10 11 9 14 12 14 13 O.60-1.00 m with strengthened duct In tendon section with minimum radius of curvature a distance of 0.60-0.80 m applies. 15 16 16 16 <td>Cross-sectional area</td> <td>Ø 15.3 mm</td> <td>mm²</td> <td>420</td> <td>560</td> <td>700</td> <td>840</td> <td>980</td> <td>1 12</td> <td>0 1260</td> <td>1680</td> <td>2 100</td>	Cross-sectional area	Ø 15.3 mm	mm ²	420	560	700	840	980	1 12	0 1260	1680	2 100			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	of prestressing steel	Ø 15.7 mm	mm ²	450	600	750	900	1 0 5 0	1 20	0 1350	1 800	2 250			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Nominal mass of	Ø 15.3 mm	kg/m	3.28	4.37	5.47	6.56	7.65	8.74	4 9.84	13.12	16.40			
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Round steel duct ¹⁾ Duct I Ø d/d₀ mm 40/47 45/52 50/57 55/62 65/72 65/72 75/82 80/87 Eccentricity mm 3 6 7 7 6 10 9 10 10 Duct II Ø d/d₀ mm 45/52 50/57 55/62 60/67 70/77 80/87 85/92 Eccentricity mm 5 9 10 11 9 14 12 14 13 Distance of tendon support m 5 9 10 11 9 14 12 14 13 Distance of tendon support m 5 9 10 10 10 10 10 0.60–1.80 mytimismum radius of curvature a distance of 0.60–0.80 m applies. Friction coefficient k 0.005 rad/m ≙ 0.30 °/m 430 518 6837 6843 6849 6855 Number of strands 19 22 27 31	Modulus of elasticity	Ν	I/mm ²			1	95 000	(standa	ard va	lue)					
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Round steel duct ¹⁾														
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Duct I	∅ di/da	mm	40/47	45/52	50/57	55/62	55/62	65/7	2 65/72	2 75/82	80/87			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Eccentricity		mm	3	6	7	7	6	10	9	10	10			
Eccentricity mm 5 9 10 11 9 14 12 14 13 Distance of tendon support m 0.60-1.80 m with stiffening, e.g. with strand bundle or PE tube 0.60-1.00 m with stirgethened duct 0.60-0.80 m applies. Friction coefficient μ rad1 0.60-0.80 m applies. Vobble coefficient k 0.005 rad/m ≙ 0.30 °/m Friction loss in stressing anchor % 1.0 1.0 0.8 0.8 0.7 0.7 0.5 0.5 Tendon 6819 6822 6827 6831 6837 6843 6849 6855 Number of strands 19 22 27 31 37 43 49 55 Cross-sectional area Ø 15.7 mm mm² 2850 3300 4050 4550 5550 6450 7350 8250 Nominal mass of Ø 15.3 mm kg/m 20.77 24.05 29.51 33.88 40.44 47.00 53.56 60.12 Prestressing steel	Duct II	arnothing d _i /d _a	mm	45/52	50/57	55/62	60/67	60/67	70/7	7 70/77	7 80/87	85/92			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Eccentricity		mm	5	9	10	11	9	14	12	14	13			
$\begin{tabular}{ c c c c c c c } \hline Friction coefficient μ rad-1$ 0.19 $$ $$ $$ $$ $$ $$ $$ $$ $$ $$ $$ $$ $$	Distance of tendon s	m	0.60- In ten	–1.80 m don sec	n with st 0.60–1 tion wit	iffening I.00 m v h minim 0.60–0	, e.g. w vith stre ium rac).80 m	rith stra engthe lius of applie	and bunc ened duc curvatur s.	lle or PE t e a dista	tube nce of				
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Friction coefficient μ rad ⁻¹ 0.19														
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Wobble coefficient	k					0.005 ra	ad/m ≙	0.30 °	'/m					
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Friction loss in stress	ing anchor	%	1.0	1.0	1.0	0.8	0.8	0.7	0.7	0.5	0.5			
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$				<u> </u>											
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Tendon														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				6819	6822	682	7 68	31 6	837	6843	6849	6855			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Number of strands			6819 19	6822 22	682 27	7 68	31 6 1	837 37	6843 43	6849 49	6855 55			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Number of strands Cross-sectional area	Ø 15.3 mm	mm ²	6819 19 2660	6822 22 3 080	682 27 378	7 68 3 3 0 43	31 6 1 40 5	837 37 180	6843 43 6 020	6849 49 6 860	6855 55 7 700			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Number of strands Cross-sectional area of prestressing steel	Ø 15.3 mm Ø 15.7 mm	mm ² mm ²	6819 19 2660 2850	6822 22 3 080 3 300	682 27 378 405	7 68 3 3 0 43 0 46	31 6 1 40 5 50 5	837 37 180 550	6843 43 6 020 6 450	6849 49 6 860 7 350	6855 55 7 700 8 250			
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Number of strands Cross-sectional area of prestressing steel Nominal mass of	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm	mm ² mm ² kg/m	6819 19 2 660 2 850 20.77	6822 22 3 080 3 300 24.05	682 27 378 405 29.5	7 68 3 3 0 43 0 46 1 33.	31 6 1	837 37 180 550 0.44	6843 43 6 020 6 450 47.00	6849 49 6 860 7 350 53.56	6855 55 7700 8250 60.12			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm Ø 15.7 mm	mm ² mm ² kg/m kg/m	6819 19 2 660 2 850 20.77 22.27	6822 22 3 080 3 300 24.05 25.78	682 27 378 405 29.5 31.6	7 68 3 0 43 0 43 0 1 33. 34 36.	31 6 1	837 37 180 550 0.44 3.36	6843 43 6 020 6 450 47.00 50.40	6849 49 6 860 7 350 53.56 57.43	6855 55 7700 8250 60.12 64.46			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm Ø 15.7 mm N	mm ² mm ² kg/m kg/m	6819 19 2 660 2 850 20.77 22.27	6822 22 3 080 3 300 24.05 25.78	682 27 378 405 29.5 31.6	7 68 0 43 0 46 1 33. 4 36. 195 000	31 6 1	837 37 180 550 0.44 3.36 ard va	6843 43 6 020 6 450 47.00 50.40 lue)	6849 49 6 860 7 350 53.56 57.43	6855 55 7700 8250 60.12 64.46			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity Round steel duct ¹⁾	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm Ø 15.7 mm N	mm ² mm ² kg/m kg/m	6819 19 2 660 2 850 20.77 22.27	6822 22 3 080 3 300 24.05 25.78	682 27 378 405 29.5 31.6	7 68 0 43 0 46 1 33. 4 36. 195 000	31 6 1	837 37 180 550 0.44 3.36 ard va	6843 43 6 020 6 450 47.00 50.40 lue)	6849 49 6 860 7 350 53.56 57.43	6855 55 7700 8250 60.12 64.46			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity Round steel duct ¹⁾ Duct I	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm Ø 15.7 mm N Ø di/da	mm ² mm ² kg/m kg/m l/mm ² mm	6819 19 2660 2850 20.77 22.27 90/97	6822 22 3 080 3 300 24.05 25.78 95/102	682 27 378 405 29.5 31.6 1 2 105/1	7 68: 3 0 43 0 46 33. 1 33. 4 36 36. 36. 195 000 12 115/	31 6 1	837 37 180 550 0.44 3.36 ard va	6843 43 6 020 6 450 47.00 50.40 lue)	6849 49 6 860 7 350 53.56 57.43	6855 55 7700 8250 60.12 64.46			
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity Round steel duct ¹⁾ Duct I Eccentricity	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm Ø 15.7 mm N Ø di/da	mm ² mm ² kg/m kg/m l/mm ² mm mm	6819 19 2 660 2 850 20.77 22.27 90/97 10	6822 22 3 080 3 300 24.05 25.78 95/102 10	682 27 378 405 29.5 31.6 2105/1 11	7 68: 3 0 43 0 46 33. 1 33. 4 195 000 12 115/ 12 115/ 1	31 6 1 5 40 5 50 5 88 4 33 4 (standa) 122 5	837 37 180 550 0.44 3.36 ard va	6843 43 6 020 6 450 47.00 50.40 lue)	6849 49 6 860 7 350 53.56 57.43	6855 55 7700 8250 60.12 64.46			
$ \begin{array}{c} 1.00-1.80 \text{ m with stiffening, e.g. with PE tube} \\ 0.80-1.50 \text{ m with strengthened duct} \\ \text{In tendon section with minimum radius of curvature a distance of} \\ 0.80-1.20 \text{ m applies.} \\ \hline \text{Friction coefficient} & \mu & \text{rad}^{-1} & 0.19 \\ \hline \text{Wobble coefficient} & k & 0.005 \text{ rad/m} \triangleq 0.30 \text{ °/m} \\ \hline \text{Friction loss in stressing anchor} & \% & 0.5 \\ \hline \end{array} $	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity Round steel duct ¹⁾ Duct I Eccentricity Duct II	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm Ø 15.7 mm N Ø di/da Ø di/da	mm ² mm ² kg/m kg/m J/mm ² mm mm	6819 19 2 660 2 850 20.77 22.27 90/97 10 95/102	6822 22 3 080 3 300 24.05 25.78 95/102 10 105/11	682 27 378 405 29.5 31.6 2 2 105/1 2 115/1	7 68 0 43 0 46 31 33. 34 36. 195 000 12 115/ 12 121	31 6 1 - 40 5 50 5 88 4 33 4 (standa) 122 5 127	837 37 180 550 0.44 3.36 ard va 	6843 43 6 020 6 450 47.00 50.40 lue) 140/147	6849 49 6 860 7 350 53.56 57.43 	6855 55 7700 8250 60.12 64.46 			
$\begin{tabular}{ c c c c } \hline Friction coefficient & μ & rad^{-1} & 0.19 \\ \hline Wobble coefficient & k & $0.005 \ rad/m $\triangleq $0.30 \ ^\circ/m$ \\ \hline Friction loss in stressing anchor & $\%$ & 0.5 \\ \hline \end{tabular}$	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity Round steel duct ¹⁾ Duct I Eccentricity Duct II Eccentricity	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm Ø 15.7 mm N Ø di/da Ø di/da	mm ² mm ² kg/m kg/m J/mm ² mm mm mm	6819 19 2 660 2 850 20.77 22.27 90/97 10 95/102 14	6822 22 3 080 3 300 24.05 25.78 95/102 10 105/11 18	682 27 378 405 29.5 31.6 1 2 2 105/1 2 105/1 2 115/1 18	7 68: 3 0 43 0 46 33. 4 36. 95 000 12 115/ 15 22 120/ 1	31 6 1	837 37 180 550 0.44 3.36 ard va 0/137 17	6843 43 6 020 6 450 47.00 50.40 lue) 140/147 19	6849 49 6 860 7 350 53.56 57.43 150/157 21	6855 55 7700 8250 60.12 64.46 160/167 23			
Wobble coefficientk $0.005 \text{ rad/m} \triangleq 0.30 \degree/\text{m}$ Friction loss in stressing anchor% 0.5	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity Round steel duct ¹⁾ Duct I Eccentricity Duct II Eccentricity Distance of tendon supervision	Ø 15.3 mm Ø 15.7 mm Ø 15.3 mm Ø 15.7 mm Ø di/da Ø di/da	mm ² kg/m kg/m l/mm ² mm mm mm mm	6819 19 2 660 2 850 20.77 22.27 90/97 10 95/102 14 In ten	6822 22 3 080 3 300 24.05 25.78 95/102 10 105/11 18 1.00 don sec	682 27 378 405 29.5 31.6 2105/1 2105/1 2115/1 2115/1 18 0-1.80 1 0.80-1 ction wit	7 68: 3 0 43 0 46 33. 1 33. 436. 195 000 12 115/ 12 115/ 13 22 120/ 13 1.50 m with s 1.50 m with s 1.50 m v 1.50 m v	31 6 1 5 40 5 50 5 88 4 33 4 (standa) 122 5 127 5 127 5 127 37 5 127 137 127 137 127 127 127 127 127 127 127 127 127 130 7 127 132 132 133 133 133 134 135 136 137	837 37 180 550 0.44 3.36 ard va 0/137 17 g, e.g engthe lius of applie	6843 43 6 020 6 450 47.00 50.40 lue) 140/147 19 . with PE ened duc curvatur s.	6849 49 6 860 7 350 53.56 57.43 	6855 55 7700 8250 60.12 64.46 160/167 23 nce of			
Friction loss in stressing anchor % 0.5	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity Round steel duct ¹⁾ Duct I Eccentricity Duct II Eccentricity Distance of tendon superimediation Friction coefficient	<u>Ø 15.3 mm</u> <u>Ø 15.7 mm</u> <u>Ø 15.3 mm</u> <u>Ø 15.7 mm</u> <u>Ø di/da</u> <u>Ø di/da</u> upport	mm ² kg/m kg/m J/mm ² mm mm mm mm mm	6819 19 2 660 2 850 20.77 22.27 90/97 10 95/102 14 In ten	6822 22 3 080 3 300 24.05 25.78 95/102 10 105/11 18 1.00 don sec	682 27 378 405 29.5 31.6 1 2105/1 2105/1 2115/1 2115/1 18 0-1.80 (0.80-1 0.80-1	7 68: 0 4 3 0 4 6 31 33. 34 36. 195 000 12 12 115/ 22 120/ 1 1 12 1.50 m v h minim 0.80-1	31 6 1 40 5 50 5 88 4 33 4 (standation of the stress of t	837 37 180 550 0.44 3.36 ard va 0/137 17 g, e.g engthe lius of applie	6843 43 6 020 6 450 47.00 50.40 lue) 140/147 19 . with PE ened duc curvatur s.	6849 49 6 860 7 350 53.56 57.43 150/157 21 tube t re a dista	6855 55 7700 8250 60.12 64.46 160/167 23 nce of			
	Number of strands Cross-sectional area of prestressing steel Nominal mass of prestressing steel Modulus of elasticity Round steel duct ¹⁾ Duct I Eccentricity Duct II Eccentricity Distance of tendon su Friction coefficient Wobble coefficient	<u>Ø 15.3 mm</u> <u>Ø 15.7 mm</u> <u>Ø 15.3 mm</u> <u>Ø 15.7 mm</u> <u>Ø di/da</u> <u>Ø di/da</u> upport <u>μ</u> k	mm ² kg/m kg/m I/mm ² mm mm mm mm mm	6819 19 2 660 2 850 20.77 22.27 90/97 10 95/102 14 In ten	6822 22 3 080 3 300 24.05 25.78 95/102 10 105/11 18 1.00 don sec	682 27 378 405 29.5 31.6 2105/1 2105/1 2105/1 2105/1 11 2115/1 0.80-1 0.80-1 ction wit	7 68: 0 4.3 0 4.6 1 33. 14 36. 195 000 12 12 115/ 22 120/ 1 1 50 m v 1 h minim 0.80-1 0.005 ra 0.005 ra	31 6 1 40 5 50 5 88 4 33 4 (standard) 122 5 127 13 7 127 13 7 127 130 7 0.19 ad/m ≙	837 37 180 550 0.44 3.36 ard va 0/137 17 g, e.g engthe lius of applie 0.30 °	6843 43 6 020 6 450 47.00 50.40 lue) 140/147 19 . with PE ened duc curvatur s.	6849 49 6 860 7 350 53.56 57.43 150/157 21 tube t e a dista	6855 55 7 700 8 250 60.12 64.46 160/167 23 nce of			

Friction and wobble coefficients for round plastic duct see Clause 1.5.



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Bonded prestressing system

DYWIDAG – Strand

Annex 3

Technical data Tendons 6803 to 6855 with round steel duct of European Technical Assessment

ETA-13/0815 of 29.01.2021







Tendon				6803	6804	6805				
Number of strands				3	4	5				
Cross-sectional area of	Ø 15.3	3 mm	mm ²	420	560	700				
prestressing steel	Ø 15.7	' mm	mm²	450	600	750				
Nominal mass of	Ø 15.3	8 mm	kg/m	3.28	4.37	5.47				
prestressing steel	Ø 15.7	' mm	kg/m	3.52	4.69	5.86				
Modulus of elasticity			N/mm ²	195 000	(standar	d value)				
Flat steel duct ¹⁾										
Dimonoiono		di	mm	55 imes 21	70 imes 21	85 × 21				
Dimensions	_	d_{a}	mm	60 imes 25	75 imes 25	90 imes 25				
Trumpet length		m₀	mm	350	350	500				
Distance of tendon suppo	ort		m	0.50-1.00						
Wobble coefficient		k		0.010 r	ad/m ≙ 0	.60 °/m				
Bending around weak ax Minimum radius of curvation	is, ture	R_{min}	m		2.5					
Friction coefficient		μ	rad⁻¹	0.15						
Bending around strong a Minimum radius of curva	R_{min}	m	5.0							
Friction coefficient		μ	rad ⁻¹	0.23	0.26	0.32				

¹⁾ Friction and wobble coefficients for flat plastic duct see Clause 1.5.



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Bonded prestressing system

DYWIDAG – Strand

Technical data Tendons 6803 to 6805 with flat steel duct Annex 4

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of European Technical Assessment



	Maximum prestressing and overstressing forces for strand 140 mm ²										
		Cross-	f _{pk} = 1 77	'0 N/mm ²	$f_{pk} = 1.860 \text{ N/mm}^2$						
Number of strands ¹⁾	Mass of strands	sectional area of strands	Maximum prestressing force ^{2), 4)}	Maximum over- stressing force ^{2), 3), 4)}	Maximum prestressing force ^{2), 4)}	Maximum over- stressing force ^{2), 3), 4)}					
		Ap	$0.90 \cdot F_{p0.1}$ ⁵⁾	0.95 · F _{p0.1}	$0.90 \cdot F_{p0.1}$ ⁵⁾	0.95 · F _{p0.1}					
	kg/m	mm ²	kN	kN	kN	kN					
1	1.09	140	197	208	207	218					
3	3.28	420	590	622	620	654					
4	4.37	560	786	830	827	872					
5	5.47	700	983	1037	1 033	1 091					
6	6.56	840	1 179	1 245	1 240	1 309					
7	7.65	980	1 376	1 452	1 446	1 527					
8	8.74	1 120	1 572	1 660	1 653	1 745					
9	9.84	1 260	1 769	1 867	1 860	1 963					
12	13.12	1 680	2 359	2 4 9 0	2 480	2617					
15	16.40	2 100	2 948	3 1 1 2	3 100	3 272					
19	20.77	2 660	3 735	3 942	3 926	4 144					
22	24.05	3 080	4 324	4 565	4 546	4 799					
27	29.51	3 780	5 307	5 602	5 579	5 889					
31	33.88	4 340	6 093	6 4 3 2	6 406	6 762					
37	40.44	5 180	7 273	7 677	7 646	8 070					
43	47.00	6 0 2 0	8 452	8 922	8 886	9 379					
49	53.56	6 860	9631	10 167	10 125	10 688					
55	60.12	7 700	10 811	11 4 1 1	11 365	11 997					

¹⁾ By omitting strands, tendons with number of strands between the numbers given may be installed. The respective prestressing force is reduced per omitted strand as specified for one strand.

²⁾ The given values are maximum values according to Eurocode 2. The actual values are taken from the standards and regulations in force at the place of use.

- ³⁾ Overstressing is permitted if the force in the prestressing jack can be measured to an accuracy of \pm 5 % of the final value of the overstressing force.
- ⁴⁾ For prestressing steel strands according to prEN 10138-3, 09.2000, the values are multiplied by 0.98.

⁵⁾ Maximum prestressing force P_{0, max}

Where

 f_{pk} Characteristic tensile strength of prestressing steel strand

 $F_{p0.1}$ Characteristic value of 0.1 % proof force of tendon, $F_{p0.1}$ = $A_p\cdot f_{p0.1}$

For $F_{p0.1}$ of one single prestressing steel strand see Annex 26.



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Bonded prestressing system DYWIDAG – Strand

Maximum prestressing and overstressing forces for prestressing steel strand 140 mm²

Annex 5

of European Technical Assessment **ETA-13/0815** of 29.01.2021



	Maximum prestressing and overstressing forces for strand 150 mm ²										
		Cross-	f _{pk} = 1 77	'0 N/mm ²	f _{pk} = 1 86	60 N/mm²					
Number of strands ¹⁾	Mass of strands	sectional area of strands	Maximum prestressing force ^{2), 4)}	Maximum over- stressing force ^{2), 3), 4)}	Maximum prestressing force ^{2),4)}	Maximum over- stressing force ^{2), 3), 4)}					
		Ap	$0.90 \cdot F_{p0.1}$ ⁵⁾	0.95 · F _{p0.1}	$0.90 \cdot F_{p0.1}$ ⁵⁾	0.95 · F _{p0.1}					
	kg/m	mm ²	kN	kN	kN	kN					
1	1.17	150	211	222	221	234					
3	3.52	450	632	667	664	701					
4	4.69	600	842	889	886	935					
5	5.86	750	1 053	1 112	1 107	1 169					
6	7.03	900	1 264	1 334	1 328	1 402					
7	8.20	1 050	1 474	1 556	1 550	1 636					
8	9.38	1 200	1 685	1 778	1 771	1 870					
9	10.55	1 350	1 895	2 001	1 993	2 103					
12	14.06	1 800	2 527	2 668	2 657	2 804					
15	17.58	2 250	3 159	3 335	3 321	3 506					
19	22.27	2 850	4 001	4 224	4 207	4 440					
22	25.78	3 300	4 633	4 891	4 871	5 141					
27	31.64	4 050	5 686	6 002	5978	6 310					
31	36.33	4 650	6 529	6 891	6 863	7 245					
37	43.36	5 550	7 792	8 225	8 192	8 647					
43	50.40	6 4 5 0	9 0 5 6	9 559	9 520	10 049					
49	57.43	7 350	10 319	10 893	10 849	11 451					
55	64.46	8 250	11 583	12 227	12 177	12 854					

¹⁾ By omitting strands, tendons with number of strands between the numbers given may be installed. The respective prestressing force is reduced per omitted strand as specified for one strand.

²⁾ The given values are maximum values according to Eurocode 2. The actual values are taken from the standards and regulations in force at the place of use.

- ³⁾ Overstressing is permitted if the force in the prestressing jack can be measured to an accuracy of \pm 5 % of the final value of the overstressing force.
- ⁴⁾ For prestressing steel strands according to prEN 10138-3, 09.2000, the values are multiplied by 0.98.

⁵⁾ Maximum prestressing force P_{0, max}

Where

 f_{pk} Characteristic tensile strength of prestressing steel strand

 $F_{p0.1}$ Characteristic value of 0.1 % proof force of tendon, $F_{p0.1}$ = $A_p\cdot f_{p0.1}$

For $F_{p0.1}$ of one single prestressing steel strand see Annex 26.



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Bonded prestressing system DYWIDAG – Strand

Maximum prestressing and overstressing forces for prestressing steel strand 150 mm²

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-												
	Strand Y1	860S7, A _p :	= 140 mm	2	9	Strand Y18	860S7, A _p :	= 150 mm	2			
Number of strands	Duct I	Minimum radius of curvature	Duct II	Minimum radius of curvature	Number of strands	Duct I	Minimum radius of curvature	Duct II	Minimum radius of curvature			
n	$arnothing d_i$	R _{min}	$arnothing d_i$	R _{min}	n	$arnothing {f d}_i$	R _{min}	$arnothing d_i$	R _{min}			
—	mm	m	mm	m	_	mm	m	mm	m			
1	20	2.0	25	2.0	1	20	2.0	25	2.0			
3	40	3.7	45	3.0	3	40	4.0	45	3.2			
4	45	3.8	50	3.4	4	45	4.1	50	3.8			
5	50	4.3	55	3.9	5	50	4.7	55	4.3			
6	55	4.7	60	4.3	6	55	5.1	60	4.7			
7	55	5.4	60	5.0	7	55	6.0	60	5.5			
8	65	5.3	70	4.9	8	65	5.8	70	5.4			
9	65	5.9	70	5.5	9	65	6.5	70	6.0			
12	75	6.8	80	6.4	12	75	7.5	80	7.0			
15	80	8.0	85	7.5	15	80	8.8	85	8.3			
19	90	9.0	95	8.5	19	90	9.9	95	9.4			
22	95	9.9	105	8.9	22	95	10.9	105	9.8			
27	105	11.0	115	10.0	27	105	12.1	115	11.0			
31	115	11.5	120	11.0	31	115	12.6	120	12.1			
37			130	12.1	37	_		130	13.3			
43			140	13.1	43			140	14.4			
49			150	13.9	49			150	15.3			
55			160	14.7	55			160	16.1			

Minimum radii of curvature for $p_{R, max} = 140 \text{ kN/m}$, prestressing steel strand Y1860S7 ¹) with use of corrugated steel ducts according to EN 523

¹⁾ Minimum radii of curvature for prestressing steel strand Y1770S7 can be calculated with the equation in Clause 1.7.



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Bonded prestressing system DYWIDAG – Strand

Minimum radii of curvature $p_R = 140 \text{ kN/m}$

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	Strand Y1	860S7, A _p :	= 140 mm	2		Strand Y1	860S7, A _p :	= 150 mm	2				
Number of strands	Duct I	Minimum radius of curvature	Duct II	Minimum radius of curvature	Number of strands	Duct I	Minimum radius of curvature	Duct II	Minimum radius of curvature				
n	$\oslash \mathbf{d}_{i}$	R _{min}	$arnothing d_i$	R _{min}	n	$arnothing d_i$	R _{min}	$arnothing \mathbf{d}_{i}$	R _{min}				
	mm	m	mm	М		mm	m	mm	m				
1	20	2.0	25	2.0	1	20	2.0	25	2.0				
3	40	2.6	45	2.2	3	40	2.8	45	2.3				
4	45	2.7	50	2.4	4	45	2.8	50	2.6				
5	50	3.0	55	2.7	5	50	3.3	55	3.0				
6	55	3.3	60	3.0	6	55	3.6	60	3.3				
7	55	3.8	60	3.5	7	55	4.2	60	3.8				
8	65	3.7	70	3.4	8	65	4.0	70	3.8				
9	65	4.1	70	3.8	9	65	4.5	70	4.2				
12	75	4.8	80	4.5	12	75	5.3	80	4.9				
15	80	5.6	85	5.3	15	80	6.2	85	5.8				
19	90	6.3	95	6.0	19	90	6.9	95	6.6				
22	95	6.9	105	6.3	22	95	7.6	105	6.9				
27	105	7.7	115	7.0	27	105	8.4	115	7.7				
31	115	8.0	120	7.7	31	115	8.8	120	8.5				
37			130	8.5	37	_		130	9.3				
43			140	9.2	43			140	10.1				
49			150	9.8	49			150	10.7				
55			160	10.3	55			160	11.3				

Minimum radii of curvature for $p_{R, max} = 200 \text{ kN/m}$, prestressing steel strand Y1860S7 ¹) with use of corrugated steel ducts according to EN 523

¹⁾ Minimum radii of curvature for prestressing steel strand Y1860S7 can be calculated with the equation in Clause 1.7.



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Bonded prestressing system DYWIDAG – Strand

Minimum radii of curvature $p_R = 200 \text{ kN/m}$

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	-	,
Anchorage or coupler	Slip	Locking measures
	mm	
Stressing anchor – Wedge plate	3 ¹⁾	Power-seating 20 kN per strand
 Anchor plate SD Coupler plate R 	6 ¹⁾	
Slip at stressing anchor considered for calculation of elongation	1	
Fixed anchor – Wedge plate	1	Pre-wedging with P _{0, max} , wedge keeper plate
- Anchor plate SD	5	Wedge keeper plate
Bond anchorage	0	
Fixed coupler R 2 nd construction stage	4	Spring
Movable coupler D	8	Spring

¹⁾ Slip occurs by transfer of prestressing force from jack to anchorage.



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²⁾ The external dimensions x, y have to be met exactly.



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Bonded prestressing system

DYWIDAG – Strand

Plate anchorage SD Data sheet for tendons 6803 to 6809 Dimensions in mm

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Bond anchorage H 6803 to 6809 for $f_{cm, 0, cube} \ge 34 \text{ N/mm}^2$ or $f_{cm, 0, cyl} \ge 28 \text{ N/mm}^2$ strand Y1770S7 15.3, Y1770S7 15.7, strand Y1860S7 15.3, and strand Y1860S7 15.7

For layout see the Annexes 17 and 18.

Tendon		6803	68	04	68	05	68	07	68	09
Number of stran	ds	3	2	1	Į	5	-	7	Ç	9
Format		HL	HL	HR	HL	HR	HL	HR	HL	HR
	А	290	390	210	330	210	450	250	390	290
	В	90	90	190	90	210	90	250	210	290
Dimensions	Z	1 400	1 400	1 400	1 400	1 400	1 400	1 400	1 400	1 400
	Е	950	950	950	950	950	950	950	950	950
	L	1 250	1 250	1 250	1 250	1 250	1 250	1 250	1 250	1 250
Holiv	$\oslash d_a{}^{\star}$				160	160	180	180	230	230
	$\varnothingd_s{}^{\star}$				12	12	12	12	14	14
	ØV			D	uct outer	diamete	r + ~ 3 m	im	_	
Ring	0	11	14	14	14	14	14	14	14	14
	Ι	20	20	20	20	20	30	30	30	30
Minimum contro	a _x	180	190	285	210	305	230	340	280	375
and edge	ay	380	430	285	440	305	500	340	500	375
distance	r _x	80	85	135	95	145	105	160	130	180
	r _y	180	205	135	210	145	240	160	240	180
	а	100	100		100		100		100	100
Bursting	b	80	80		80		83		90	100
stirrups ¹⁾	n ₀	6	6	—	6		6	—	6	5
	Ø	10	10		10		10		12	14
Width		160	170		190		210		260	355
Height		150	180		180		180		200	120
	С	115	115	115	115	105	115	105	120	120
Stirrup 1	d	80	80	80	80	80	83	85	90	100
Surrup	n ₁	8	8	7	8	7	8	7	8	6
	Ø	12	12	12	12	12	12	12	14	14
Width		160	170	265	190	285	210	320	260	355
Height		360	410	265	420	285	480	320	480	355
	е	850	850	785	850	785	850	785	900	810
Stirrup 2	f	166	166	170	166	170	166	170	200	185
	n ₂	5	5	5	5	5	5	5	4	5
	Ø	12	12	12	12	12	12	12	14	14
Width		160	170	265	190	285	210	320	260	355
Height		360	410	265	420	285	480	320	480	355

¹⁾ Crosswise installation of bursting reinforcement for fixed anchor HR according to Annex 18

Dimensions in mm



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Bonded prestressing system DYWIDAG – Strand

Bond anchorage H Data sheet for tendons 6803 to 6809 Annex 19

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Bond anchorage H 6812 to 6822 for $f_{cm, 0, cube} \ge 34 \text{ N/mm}^2$ or $f_{cm, 0, cyl} \ge 28 \text{ N/mm}^2$ strand Y1770S7 15.3, Y1770S7 15.7, strand Y1860S7 15.3, and strand Y1860S7 15.7

For layout see the Annexes 17 and 18.

Tendon		68	12	68	15	68	19	68	22
Number of stran	ds	1	2	1	5	1	9	2	2
Format		HL	HR	HL	HR	HL	HR	HL	HR
	А	480	390	480	410	610	490	730	490
	В	250	330	250	350	250	390	250	450
Dimensions	Z	1 400	1 400	1 400	1 400	1 400	1 400	1 400	1 400
	E	950	950	950	950	950	950	800 ²⁾	950
	L	1 250	1 250	1 250	1 250	1 250	1 250	1 250	1 250
Holix	$arnothing d_{a}^{\star}$	250	250	295	295	330	330	360	360
пеііх	$arnothing d_{s}^{\star}$	14	14	16	16	16	16	16	16
	ØV			Duct	outer diar	neter + ~	3 mm		
Ring	0	20	20	20	20	20	20	20	20
	1	30	30	30	30	30	30	30	30
	a _x	300	390	350	460	390	525	410	570
Minimum centre	ay	570	440	630	475	715	525	780	560
and edge distan	ce r _x	140	185	165	220	185	255	195	275
		275	210	305	230	350	255	380	270
	A	100	100	100	100	110	110	110	120
Bursting stirrups	1) B	100	100	100	100	110	110	110	120
	n ₀	6	5	6	6	6	5	6	5
	Ø	12	12	14	14	14	14	14	14
V	/idth	280	420	330	455	370	505	390	550
He	eight	200	150	220	230	220	230	260	280
	С	120	120	120	120	130	130	130	140
Stirrup 1	d	100	100	100	100	110	110	110	120
	n ₁	8	6	8	6	7	6	6	5
	Ø	14	14	14	14	14	14	14	14
N. N	/idth	280	370	330	440	370	505	390	550
He He	eight	550	420	610	455	695	505	760	540
	e	1 0 2 0	820	1020	900	1 1 1 2 0	1 000	1 120	1 060
Stirrup 2	t	200	200	150	150	110	120	110	120
- I.	n ₂	3	4	5	5	5	6	5	6
	Ø	14	14	14	14	14	14	14	14
M	/idth	280	370	330	440	370	505	390	550
He	eight	550	420	610	455	695	505	760	540

¹⁾ Crosswise installation of bursting reinforcement for fixed anchor HR according to Annex 18 ²⁾ Bond head in 3rd position

Dimensions in mm

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Bonded prestressing system DYWIDAG – Strand

Bond anchorage H Data sheet for tendons 6812 to 6822 Annex 20

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Bonded prestressing system

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Fixed coupler R Data sheet for tendons 6805 to 6837

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Dimensions in mm

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Assembly of movable coupler D

Bonded prestressing system

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Duct

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mm

mm

mm

100

110

f_D**

 I_{D}

Coupler tube

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Bonded prestressing system **DYWIDAG – Strand**

125

140

160

180

120

Movable coupler D Data sheet for tendons 6803 to 6837

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165

225

190

250

190

250

136

200

152

225



Designation	Specification	Material ¹⁾
Wedge	EN 10277	Steel
Wedge plate	EN ISO 683-1	Steel
Anchor plate SD	EN ISO 683-1	Steel
Coupler plate R	EN ISO 683-1	Steel
Coupler D barrel chuck	EN ISO 683-1	Steel
Coupler D fitting bolt	EN 10025-2	Steel
Anchor body MA	EN 1563	Ductile cast iron
Duct, Telescopic duct	EN 523	Steel
Coupler tube	EN 523	Steel
Duct sleeve,	EN 10130	Steel
Sleeve tube	EN ISO 17855-1	PE-HD
Trumpet	EN 10130 EN ISO 17855-1	Steel PE-HD
Helix	_	Ribbed reinforcing steel, $R_e \geq 500 \text{ N/mm}^2$
	EN 10025-2	Plain round steel
dditional reinforcement		Ribbed reinforcing steel, $R_e \geq 500 \text{ N/mm}^2$
Ring	EN 10025-2	Steel
Wedge keeper plate	EN 10025-2	Steel
Spacer	EN ISO 17855-1	PE-HD
Grout cap	EN 10130	Steel
Sealing	_	Synthetic caoutchouc

¹⁾ Detailed material specifications are deposited at Österreichisches Institut für Bautechnik



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Material specifications

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Prestressing steel strand			Y1770S7 Y1860S		60S7	
Characteristic tensile strength	R _m	N/mm ²	17	70	18	60
Nominal diameter of strand	D	mm	15.3	15.7	15.3	15.7
Nominal diameter of outer wire	do	mm	5.0	5.2	5.0	5.2
Diameter of core wire	ď	mm		≥ 1.0	3 · d₀	
Nominal mass per metre	М	g/m	1 093	1 172	1 093	1 172
Nominal cross-sectional area	Ap	mm ²	140	150	140	150
Characteristic value of maximum force	F _m	kN	248	266	260	279
Maximum value of maximum force	$F_{m,max}$	kN	285	306	299	321
Characteristic value of 0.1% proof force ¹⁾	F _{p0.1}	kN	218	234	229	246
Minimum elongation at maximum force, $L_0 \geq 500 \mbox{ mm}$	A _{gt}	%		3	.5	
Modulus of elasticity	E	N/mm ²		195 (000 ²⁾	
Relaxation after 1 000 h, for an initial force of $-0.70 \cdot F_{ma}$ - 0.80 $\cdot F_{ma}$		% %		≤ 2 ≤ 4	2.5 4.5	

¹⁾ For prestressing steel strand according to prEN 10138-3, 09.2000, the value is multiplied by 0.98.

2) Standard value

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Bonded prestressing system DYWIDAG – Strand

Specifications of the 7-wire prestressing steel strands

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	Prestressing steel strand $A_p = 140 \text{ mm}^2$ Prestressing steel strand				strand $A_p = r$	150 mm²		
Number of strands	N.A. 1)	A 2)	Y1770S7	Y1860S7	N.4.1)	▲ 2)	Y1770S7	Y1860S7
otrando	IVI ''	A _p -/	F _{pk} ³⁾	F _{pk} ³⁾	IVI ''	Ap ²	F _{pk} ³⁾	F _{pk} ³⁾
	kg/m	mm ²	kN	kN	kg/m	mm ²	kN	kN
1	1.09	140	248	260	1.17	150	266	279
3	3.28	420	744	780	3.52	450	798	837
4	4.37	560	992	1 040	4.69	600	1 064	1 1 16
5	5.47	700	1 240	1 300	5.86	750	1 330	1 395
6	6.56	840	1 488	1 560	7.03	900	1 596	1 674
7	7.65	980	1 736	1 820	8.20	1 050	1 862	1 953
8	8.74	1 120	1 984	2 080	9.38	1 200	2 128	2 232
9	9.84	1 260	2 232	2 340	10.55	1 350	2 394	2 511
12	13.12	1 680	2 976	3 120	14.06	1 800	3 192	3 348
15	16.40	2 100	3 720	3 900	17.58	2 250	3 990	4 185
19	20.77	2 660	4 712	4 940	22.27	2 850	5 054	5 301
22	24.05	3 080	5 456	5 720	25.78	3 300	5 852	6 138
27	29.51	3 780	6 696	7 020	31.64	4 050	7 182	7 533
31	33.88	4 340	7 688	8 060	36.33	4 650	8 246	8 649
37	40.44	5 180	9 176	9 620	43.36	5 550	9842	10 323
43	47.00	6 020	10 664	11 180	50.40	6 450	11 438	11 997
49	53.56	6 860	12 152	12 740	57.43	7 350	13 034	13671
55	60.12	7 700	13 640	14 300	64.46	8 250	14 630	15 345

Characteristic maximum force of tendon, F_{pk}

¹⁾ Nominal mass of tendon

²⁾ Nominal cross-sectional area of tendon

³⁾ Characteristic maximum force of tendon



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DYWIDAG – Strand

Characteristic maximum force of tendon

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Subject / type of control		Test or control method	Criteria, if any	Minimum number of samples	Minimum frequency of control
Wedge plate	Material	Checking 1)	2)	100 %	continuous
Anchor plate SD, Coupler plate R,	Detailed dimensions	Testing	2)	5%, \geq 2 specimens	continuous
Barrel chuck,	Visual inspection 3)	Checking	2)	100 %	continuous
Fitting bolt	Traceability			full	
	Material	Checking 1)	2)	100 %	continuous
Anchor body MA	Detailed dimensions	Testing	2)	$3\%, \ge 2$ specimens	continuous
	Visual inspection 3)	Checking	2)	100 %	continuous
	Traceability			full	
	Material	Checking 1)	2)	100 %	continuous
	Treatment, hardness	Testing	2)	0.5 %, $\ge 2 \text{ specimens}$	continuous
Wedge	Detailed dimensions	Testing	2)	5 %, \ge 2 specimens	continuous
	Visual inspection 3)	Checking	2)	100 %	continuous
	Traceability	full			
	Material	Checking	2), 4)	100 %	continuous
Prestressing steel strand	Diameter	Testing	2)	1 sample	each coil or
	Visual inspection	Checking	2)	1 sample	every 7 tons 5)
	Material	Checking 6)	2)	100 %	continuous
Helix in plain round steel, EN 10025	Visual inspection 3)	Checking	2)	100 %	continuous
	Traceability			full	
	Material	Checking 7)	2)	100 %	continuous
Steel strip duct	Dimension	Testing	2)	3% , ≥ 2 specimens	continuous
	Traceability	full			
Cement, Admixtures, Additions of	Material	Checking 7)	2)	100 %	continuous
filling materials as per EN 447	Traceability	full			

¹⁾ Checking by means of an inspection certificate 3.1 according to EN 10204.

²⁾ Conformity with the specifications of the components

³⁾ Successful visual inspection does not need to be documented.

⁴⁾ Checking of relevant certificate, as long as the basis of "CE"-marking is not available.

 $^{\rm 5)}~$ Maximum between a coil and 7 tons is taken into account.

⁶⁾ Checking by means of at least a test report 2.2 according to EN 10204.

⁷⁾ Checking of relevan supplier	t certificate, CE marking and declaration of performance or, if basis for CE marking is not available, certificate of
Traceability full	Full traceability of each component to its raw material.
Material	Defined according to technical specification deposited by the supplier
Detailed dimensions	Measuring of all dimensions and angles according to the specification given in the test plan
Visual inspection	Main dimensions, correct marking and labelling, surface, corrosion, coating, etc.
Treatment hardness	Surface hardness, core hardness, and treatment denth



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DYWIDAG – Strand

Contents of the prescribed test plan

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Subject / type of co	ontrol	Test or control method	Criteria, if any	Minimum number of samples ¹⁾	Minimum frequency of control
Wedge plate, Anchor plate SD, Coupler plate R,	Material	Checking and testing, hardness and chemical ²⁾	3)	1	1/year
Barrel chuck,	Detailed dimensions	Testing	3)	1	1/year
Fitting bolt	Visual inspection	Checking	3)	1	1/year
	Material	Checking and testing, hardness and chemical ²⁾	3)	1	1/year
Anchor body MA	Detailed dimensions	Testing	3)	1	1/year
	Visual inspection	Checking	3)	1	1/year
	Material	Checking and testing, hardness and chemical ²⁾	3)	2	1/year
Wedge	Treatment, hardness	Checking and testing, hardness profile	3)	2	1/year
	Detailed dimensions	Testing	3)	1	1/year
	Main dimensions, surface hardness	Testing	3)	5	1/year
	Visual inspection	Checking	3)	5	1/year
Single tensile element test		According EAD 160004-00 Annex C.	to D-0301, 7	9	1/year

¹⁾ If the kits comprise different kinds of anchor heads e.g. with different materials, different shape, different wedges, etc., then the number of samples is understood as per kind.

²⁾ Testing of hardness and checking of chemical composition by means of an inspection certificate 3.1 according to EN 10204.

³⁾ Conformity with the specifications of the components

Material Defined according to technical specification deposited by the ETA holder at the Notified body

Detailed dimensions Measuring of all dimensions and angles according to the specification given in the test plan

Visual inspection Main dimensions, correct marking and labelling, surface, corrosion, coating, etc.

Treatment, hardness Surface hardness, core hardness, and treatment depth



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Audit testing

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Reference documents

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	EAD 160004-00-0301	Post-Tensioning Kits for Prestressing of Structures					
	EAD 160027-00-0301	Special filling products for post-tensioning kits					
	Eurocodes						
	Eurocode 2	Eurocode 2 – Design of concrete structures					
	Eurocode 3	Eurocode 3 – Design of steel structures					
Eurocode 6		Eurocode 6 – Design of masonry structures					
	Standards						
	EN 206+A1, 11.2016	Concrete – Specification, performance, production and conformity					
	EN 446, 10.2007	Grout for prestressing tendons – Grouting procedures					
	EN 447, 10.2007	Grout for prestressing tendons – Basic requirements					
	EN 523, 08.2003	Steel strip sheaths for prestressing tendons – Terminology, requirements, quality control					
	EN 1563, 08.2018	Founding – Spheroidal graphite cast irons					
	EN 10025-2, 08.2019	Hot rolled products of structural steels – Part 2: Technical delivery conditions for non-alloy structural steels					
	EN 10130, 12.2006	Cold-rolled low carbon steel flat products for cold forming – Technical delivery conditions					
	EN 10204, 10.2004	Metallic products – Types of inspection documents					
	EN 10277, 06.2018	Bright steel products – Technical delivery conditions					
	EN ISO 683-1, 06.2018	Heat-treatable steels, alloy steels and free-cutting steels – Part 1: Non-alloy steels for quenching and tempering					
	EN ISO 17855-1, 10.2014	Plastics – Polyethylene (PE) moulding and extrusion materials – Part 1: Designation system and basis for specifications					
	prEN 10138-3, 09.2000	Prestressing steels – Part 3: Strand					
	prEN 10138-3, 08.2009	Prestressing steels – Part 3: Strand					
	CWA 14646, 01.2003	Requirements for the installation of post-tensioning kits for prestressing of structures and qualification of the specialist company and its personnel					



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Other documents	
98/456/EC	Commission decision 98/456/EC of 3 July 1998 on the procedure for attesting the conformity of construction products pursuant to Article 20 (2) of Council Directive 89/106/EEC as regards posttensioning kits for the prestressing of structures, OJ L 201 of 17.07.1998, p. 112
305/2011	Regulation (EU) № 305/2011 of the European Parliament and of the Council of 9 March 2011 laying down harmonised conditions for the marketing of construction products and repealing Council Directive 89/106/EEC, OJ L 088 of 04.04.2011, p. 5, amended by Commission Delegated Regulation (EU) № 568/2014 of 18 February 2014, OJ L 157 of 27.05.2014, p. 76, Commission Delegated Regulation (EU) № 574/2014 of 21 February 2014, OJ L 159 of 28.05.2014, p. 41, and Regulation (EU) 2019/1020 of the European Parliament and of the Council of 20 June 2019, OJ L 169 of 25.06.2019, p. 1
568/2014	Commission Delegated Regulation (EU) № 568/2014 of 18 February 2014 amending Annex V to Regulation (EU) № 305/2011 of the European Parliament and of the Council as regards the assessment and verification of constancy of performance of construction products, OJ L 157 of 27.05.2014, p. 76



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